

### AMENDMENTS TO THE SPECIFICATION

Please amend the paragraph that begins on page 6, line 23, and ends on page 7, line 10, of the Specification as originally filed (*i.e.*, the paragraph immediately preceding Table 1) as follows.

Preferred examples and comparative examples will now be explained with reference to Tables 1 to 3. In each of the preferred examples and comparative examples shown in Tables 1 to 3, iron powders (average particle diameter: 90  $\mu\text{m}$ ) were used as the raw powder, to which was added 0.2% by weight of ~~Lithium~~lithium stearate (average particle diameter: 5  $\mu\text{m}$ ) serving as the lubricant, which were then stirred for 30 minutes using a rotary mixer, so that 7g of the resultant mixture of the raw powder was filled into a mold forming a cylindrical column having a 1  $\text{cm}^2$  pressurization area, and then 100 compacts were successively formed at a forming pressure of 8  $\text{t/cm}^2$ . In the preferred examples, after the solution of the water-soluble lubricant dissolved in water was applied to the forming portion heated at 150deg C in the mold, it was evaporated and dried to form the crystallized layer, and then the raw powders were filled into this forming portion. In the comparative example 1, after the solution of lithium stearate (average particle diameter: 5  $\mu\text{m}$ ) dispersed in acetone was applied to the forming portion of the mold heated at 150deg C, it was evaporated and dried to form ~~the crystallized layer, a film,~~ and then the material powders were filled into this forming portion. The comparative example 2 is a case in which the lubricant was not applied to the mold. Density R in each Table shows difference between maximum and minimum values in the density of 100 compacted bodies continuously molded.